

## PHASE TRANSITIONS IN DOPED AND UNDOPED LEAD ZIRCONATE TITANATE PIEZOELECTRIC MATERIALS

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### Abstract

The study of the anelastic behaviour versus temperature at medium and low frequencies for undoped and doped lead zirconatetitanate –PZT- reveals the presence of two peaks  $P_1$  and  $P_2$ . According to the phase diagrams established for PZT materials,  $P_1$  peak could be related to the Curie transition between tetragonal ferroelectric phase and the cubic paraelectric phase, whereas the  $P_2$  peak could be related to the morphotropic phase transition between rhombohedral and tetragonal ferroelectric phases. Both  $P_1$  and  $P_2$  peaks evolutions are in accordance with several existing literature models for explaining the first order phase transition. The introduction of potassium and niobium dopants changes the nature of the phase transition process.

**Keywords:** PZT ceramics, Mechanical losses, Phase transition, Potassium doping, Niobium doping.

### Résumé

L'étude du comportement anélastique en fonction de la température aux moyennes et basses fréquences pour des Zircono-titanates de plomb –PZT non dopées et dopées révèle la présence de deux pics  $P_1$  et  $P_2$ . En se basant sur le diagramme de phase des PZT, le pic  $P_1$  peut être relié à la transition de Curie entre la phase ferroélectrique quadratique et la phase cubique paraélectrique, cependant le pic  $P_2$  peut être relié à la transition morphotropique entre les phases ferroélectriques rhomboédrique et quadratique. Les évolutions des deux pics  $P_1$  et  $P_2$  sont en bon accord avec les différents modèles existant dans la littérature et expliquant les transitions de phase du premier ordre. L'introduction des dopants potassium et niobium change la nature du processus de la transition de phase.

**Mots clés :** Céramiques PZT, Pertes mécaniques, Transition de Phase, Dopage au potassium, Dopage au niobium.

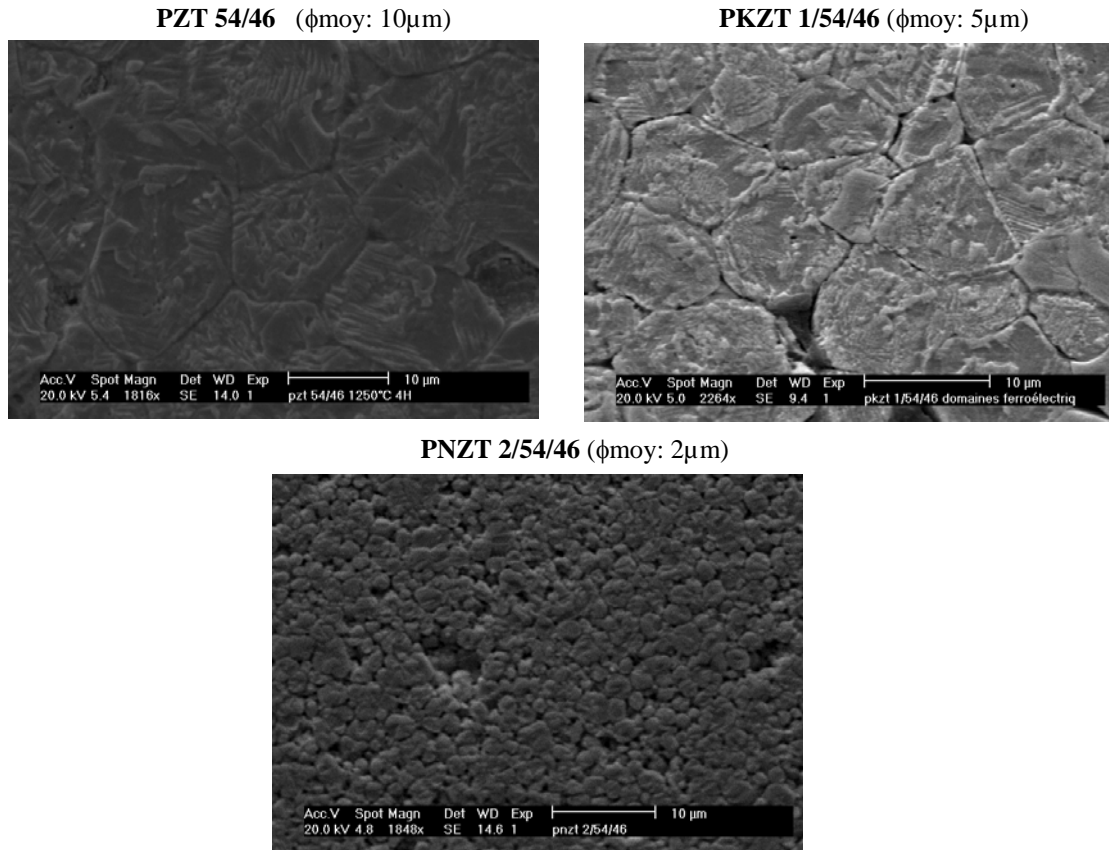
## I. INTRODUCTION

Lead zirconatetitanate piezoelectric materials are widely used as sensors and actuators in several daily applications but seldom in their simple chemical formulation. They are rather modified by the introduction of substitutionals in the A or B sites of the perovskite structure  $ABO_3$ . The role of these doping agents is generally the improvement of the materials properties for their adaptation to quite specific applications. PZT phase diagrams<sup>1-3</sup> show a zone where the rhombohedral and tetragonal ferroelectric phases coexist which is commonly called morphotropic phase boundary (MPB). Noheda et al.<sup>4,5</sup>, Ragini et al.<sup>6</sup> have reported the coexistence of also a monoclinic phase with the tetragonal phase in the MPB.

Most industrial applications are within this zone, because the majority of piezoelectric and dielectric properties present optimal values<sup>7,8</sup>.

Previous studies of the anelastic behaviour of PZT near the MPB by mechanical spectroscopy in the Hz frequency range showed relaxation phenomena due to the interaction between ferroelectric domain walls and point defects such as oxygen vacancies<sup>9,10</sup> and the presence of phase transitions<sup>11,12</sup>.

The introduction of dopant such as  $K^{1+}$  in the A-sites of the perovskite structure as a substitute for  $Pb^{2+}$  increases the oxygen vacancies concentration when oxygen ions leave their sites to maintain the electro-neutrality disturbed by the deficit charge in the A-sites. The PZT doped with an acceptor element (of lower valence) are called hard piezoelectric materials.



**Figure1.** SEM Microstructure and average grain size ( $\phi_{\text{moy}}$ ) of processed materials.

While the introduction of  $\text{Nb}^{5+}$  in substitution of the  $(\text{Zr},\text{Ti})^{4+}$  couple in the B-sites of the perovskite structure decreases the oxygen vacancies concentration. The PZT doped with a donor element (of higher valence) are called soft piezoelectric materials.

In the present paper, mechanical losses and associated Young/ Shear moduli are studied at low and medium frequencies for undoped PZT 54/46, PKZT 0.5/54/46 and PKZT 1/54/46 doped respectively with 0.5 at. % and 1 at. % of potassium, PNZT 1/54/46 and PNZT 2/54/46 doped respectively with 1 at. % and 2 at.% of niobium.

## II. MATERIALS PROCESSING AND EXPERIMENTAL PROCEDURE

By the solid reaction method undoped, potassium doped and niobium doped materials with a chemical formulation  $(\text{Zr}/\text{Ti} = 0.54/0.46)$  close to the morphotropic phase boundary (MPB) were processed. The starting powders of  $\text{PbO}$ ,  $\text{ZrO}_2$ ,  $\text{TiO}_2$  and  $(\text{K}_2\text{CO}_3$  or  $\text{Nb}_2\text{O}_5)$  are mixed and calcined at  $900^\circ\text{C}$ , the obtained powder is isostatically compacted and sintered at  $1250^\circ\text{C}$  for four hours in the presence of lead zirconate as an atmosphere powder<sup>13</sup> in order to avoid the  $\text{PbO}$  loss at high

temperatures during the sintering.

The mechanical losses  $Q^{-1}$  and Young's modulus  $M$  as function of temperature have been measured by an experimental system at medium (kilohertz range) frequencies by the transversal flexion vibration.

The mechanical losses  $Q^{-1}$  and associated shear modulus  $G$  versus temperature were measured in the Hz frequency range respectively at 1; 0.3; 0.1 Hz by using a torsion inverted pendulum, under vacuum between 25 and  $500^\circ\text{C}$  at a heating rate of  $1^\circ\text{C}/\text{min}$ . The samples for both medium and low frequencies experiments were rectangular bars with dimensions of  $40 \times 5 \times 1 \text{ mm}^3$ . More details on the measurement method could be found in our previous publications<sup>14,15</sup>.

## III. RESULTS

### III.1 Materials characterisation

The relative density and the average grain size for both processed materials are showed in **Table.1**. Both potassium and niobium have an inhibitory effect on the grain size growth (Fig.1).

X-ray patterns were carried out at room temperature with a step of  $0.05^\circ$  and a scanning speed of  $2^\circ/\text{min}$  from  $2\theta$  equal  $20^\circ$  to  $70^\circ$ . The

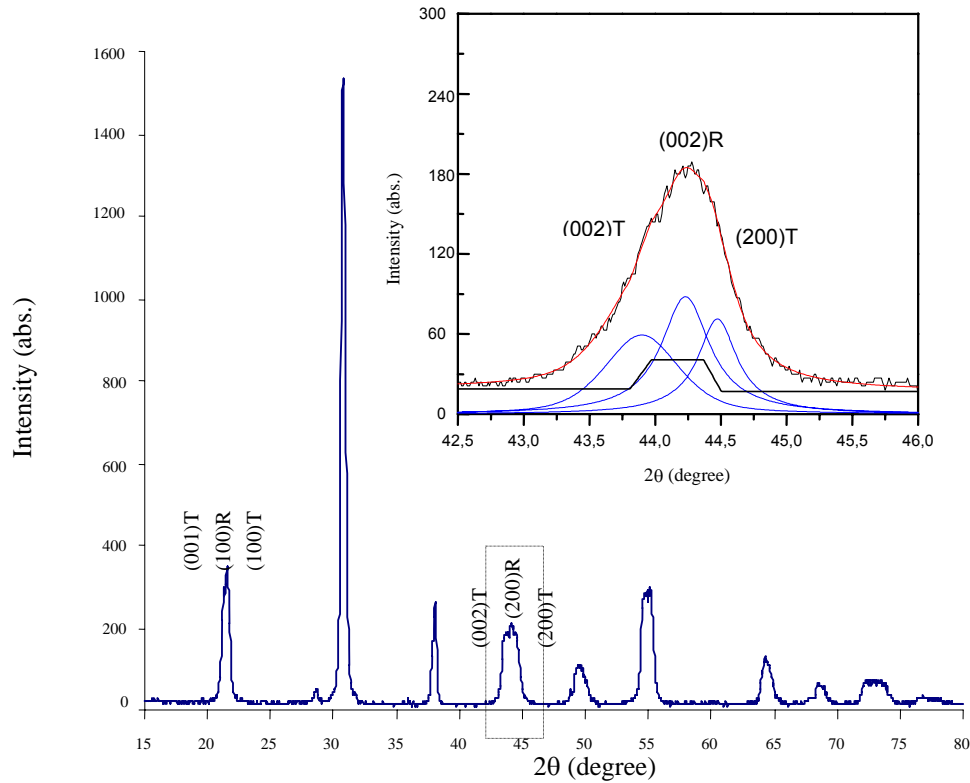


Figure 2. XRD patterns of undoped PZT.  
T : tetragonal phase ; R : rhombohedral phase

diffraction lines were split into triplets indicating the coexistence of both tetragonal and rhombohedral ferroelectric phases for both compositions as expected from the phase diagram.<sup>16,17</sup>(see Fig.2 for undoped PZT).

|             |      |   |
|-------------|------|---|
| PNZT2/54/46 | 95.8 | 2 |
|-------------|------|---|

Table 1. Relative density and average grain size for processed materials.

| Materials     | Relative Density (%) | Average grain size (µm) |
|---------------|----------------------|-------------------------|
| PZT 54/46     | 94.7                 | 10                      |
| PKZT0.5/54/46 | 94.2                 | 7                       |
| PKZT1/54/46   | 93.5                 | 5                       |
| PNZT1/54/46   | 95.2                 | 4                       |

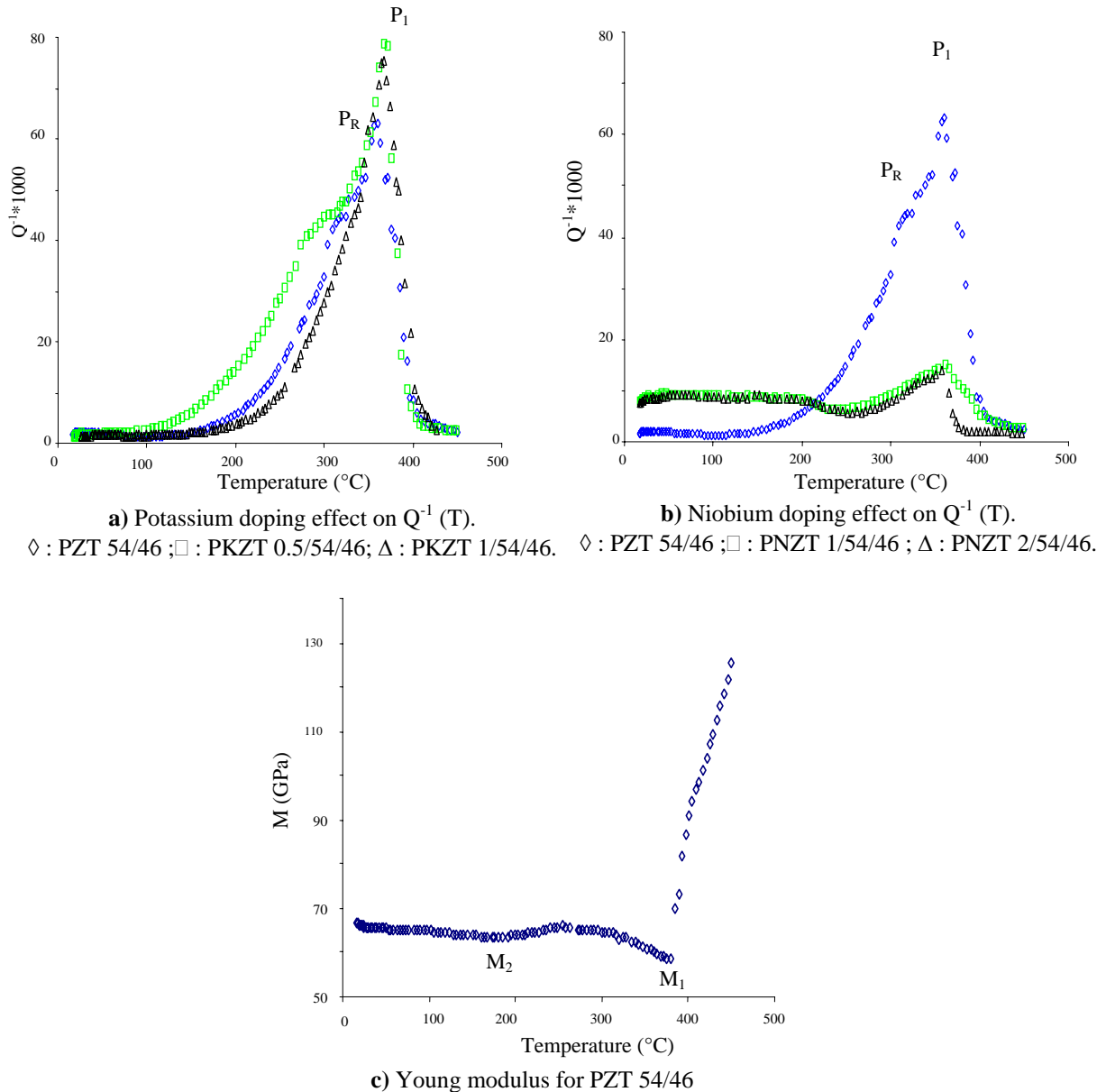
### III.2 Anelastic behaviour at medium frequencies

The mechanical losses  $Q^{-1}(T)$  and associated Young's modulus  $M(T)$  for both materials (Fig.3), show a sharp peak  $P_1$  and a corresponding Young's modulus sharp  $M_1$  minimum. The  $P_1$  peak is preceded by a  $P_R$  shoulder. No peak on the  $Q^{-1}(T)$  curve corresponds to the smooth Young's modulus  $M_2$  minimum.

According to the minima temperatures on one part and to the Jaffe phase diagram<sup>3</sup> and its revisited version<sup>14,16</sup> on the other part, the  $M_1$  minimum could be related to the Curie transition between cubic paraelectric phase and

Table 2 Phase transition temperatures deduced from  $M(T)$  curves and tetragonal  $\Delta T_{tet}$ ).

| Materials      | $T_{(C-T)}$ (°C) | $T_{(T-R)}$ (°C) | $(\Delta T_{Tetr}) = T_{C-T} - T_{T-R}$ (°C) |
|----------------|------------------|------------------|--|
| PZT 54/46      | 380              | 175              | 205  |
| PKZT 0.5/54/46 | 370              | 153              | 217  |
| PKZT 1/54/46   | 373              | 125              | 248  |
| PNZT 1/54/46   | 360              | 200              | 160  |
| PNZT 2/54/46   | 345              | 210              | 135  |



**Figure 3.** Mechanical losses  $Q^{-1}$  (T) and Young modulus  $M$  (T) measured in the medium frequency range.

tetragonal ferroelectric phase, whereas, the  $M_2$  minimum could be related to the morphotropic phase transition between tetragonal and rhombohedral ferroelectric phases. (Table.2)

### III.2.1 Potassium doping effect

The introduction of potassium increases slightly the height of the  $P_1$  peak while the peak temperature remains stable. The  $P_R$  shoulder remains stable in height, but it shifts towards the low temperatures by doping with 0.5 at. % and shifts towards high temperatures by few degrees when the potassium doping with 1 at. %. (Fig.3).

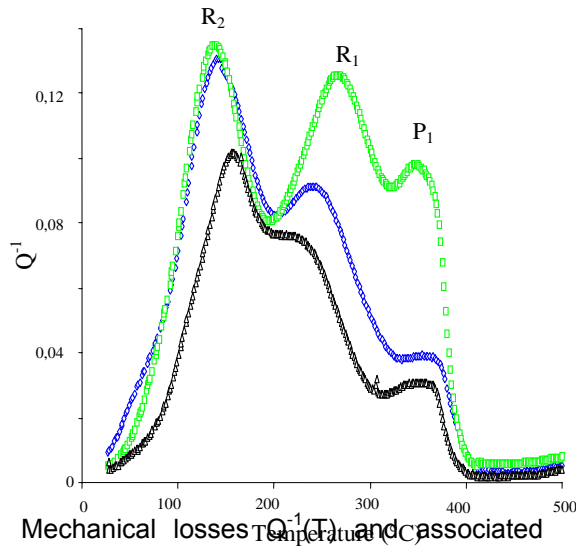
The introduction of potassium increases the width of the tetragonal ferroelectric phase range.

### III.2.2 Niobium doping effect

Niobium introduction decreases strongly the level of both  $P_1$  peak and  $P_R$  shoulder. Whereas, at temperature under 200  $^{\circ}\text{C}$  the mechanical losses of niobium doped materials are more important than those of undoped materials. (Fig.3)

The introduction of niobium decreases the width of the tetragonal ferroelectric phase range.

### III.3 Anelastic behaviour at low frequencies



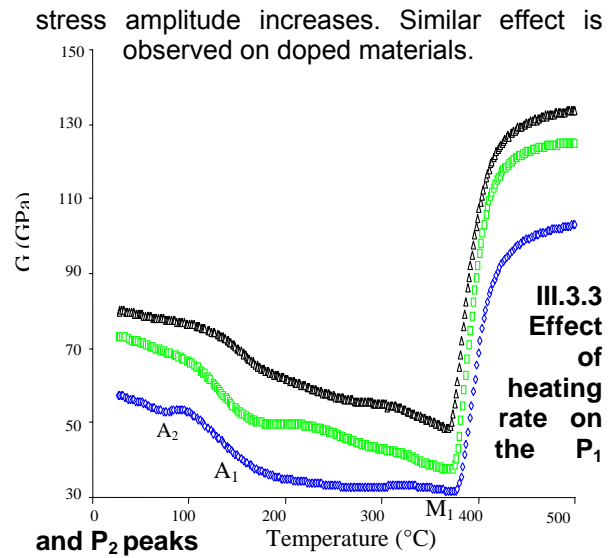
**Figure 4.** Potassium doping effect at Hz. PZT 5/46 mode. Mechanical losses  $Q^{-1}(T)$  and associated shear modulus  $G(T)$  for undoped PZT and potassium doped (Fig.4), shows the Curie transition peak  $P_1$  and its correlated modulus minimum  $M_1$ , and two other peaks  $R_1$  and  $R_2$  with two associated modulus anomalies  $A_1$  and  $A_2$ . Fig.5 for undoped PZT and niobium doped materials, shows the  $P_1$  peak and its correlated modulus minimum  $M_1$ , the  $R_1$  peak and its associated modulus anomalies  $A_1$ , and the morphotropic phase transition  $P_2$  peak – between tetragonal and rhombohedral ferroelectric phases- and its correlated modulus minimum  $M_2$ .  $R_1$  and  $R_2$  peaks are relaxation phenomena due to the interaction between ferroelectric domain walls and point defects such as oxygen vacancies<sup>9,10,15</sup>. In the present study we are interested only by the evolution of  $P_1$  and  $P_2$  peaks.

**III.3.1 Effect of frequency on the  $P_1$  and  $P_2$  peaks**

When the solicitation frequency increases, the height of both peaks decreases and they remain stable in temperature. Fig.6 shows the evolution of  $Q^{-1}_{max}(P_1)$  and  $Q^{-1}_{max}(P_2)$  as a function of the frequency inverse ( $1/f$ ) for the undoped PZT. Similar effect is observed on doped materials.

**III.3.2 Effect of stress amplitude on the  $P_1$  and  $P_2$  peaks**

Fig.7 represents the evolution of  $Q^{-1}_{max}(P_1)$  and  $Q^{-1}_{max}(P_2)$  as a function of the applied stress amplitude  $\sigma_{max}$  for the undoped PZT. The height of both  $P_1$  and  $P_2$  peaks increases when



When the heating rate increases, the height of both  $P_1$  and  $P_2$  peaks increases. Fig.8 shows the evolution of  $Q^{-1}_{max}(P_1)$  and  $Q^{-1}_{max}(P_2)$  as a function of heating rate ( $\dot{T}$ ) for the undoped PZT. Similar effect is observed on doped materials.

**IV. DISCUSSION**

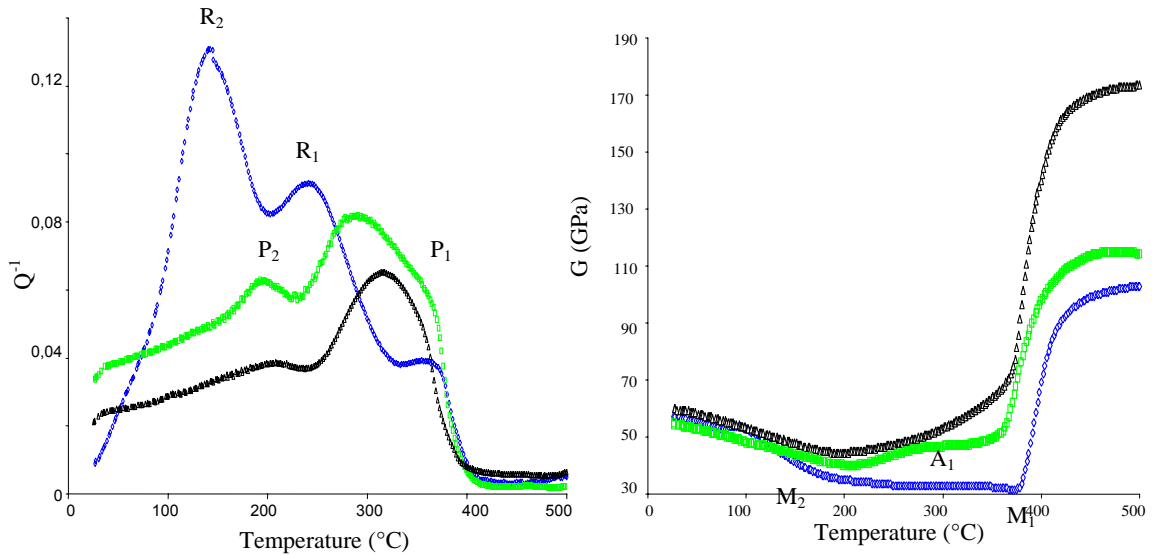
Our discussion will treat only the phase transition peaks  $P_1$  and  $P_2$ .

The height of both  $P_1$  and  $P_2$  peaks is directly proportional to stress amplitude and heating rate but inversely proportional to frequency. Such evolution is very similar to that of the first order phase transition.

Among the several theoretical models existing in literature to describe the first order phase transition reviewed by Fantozzi et al.<sup>18</sup>, one can notice a qualitative agreement of the evolution of our  $P_1$  and  $P_2$  peaks with the theoretical models of Zhang et al.<sup>19</sup>, De Jonghe et al.<sup>20</sup>

Zhang et al., proposed a model for explaining the transition peak in  $BaTiO_3$  semi-conducting materials and in which it is suggested that the mechanical losses are the result of two components:

- A transitory component, measured during heating and cooling,  $Q_t^{-1}$ . This component depends on frequency and heating rate and associated to the phase mobile interfaces.
  - An equilibrium (or stationary) component  $Q_s^{-1}$ , measured at a fixed temperature ( $\dot{T} = 0$ ) and associated to the phase immobile interfaces.
- The total internal friction is given by the following relation:



**Figure 5.** Niobium doping effect at 1Hz.  
 ◇ : PZT 54/46 ; □ : PNZT 1/54/46 ; △ : PNZT 2/54/46

$$Q^{-1} = Q_t^{-1} + Q_s^{-1} = A'(F) \alpha^2(\omega) (\dot{T}/\omega)^n + B'(F) \alpha^2(\omega) \omega \quad (1)$$

Where F is the volume fraction of the produced phase, and  $\alpha(\omega)$  could be written like following:

$$\alpha(\omega) = (2\varepsilon_0 Q^{-1}) / (\Delta M/M) = \alpha' \omega^{-P} \quad (2)$$

With  $(0 < P < 1)$

$\alpha'$  is a constant,  $\varepsilon_0$  represents the transitory phase deformation,  $\Delta M/M$  is the change in modulus. In our case, the evolution of  $Q^{-1}_{max.(P_1)}$  and  $Q^{-1}_{max.(P_2)}$  function of  $(\dot{T}/\omega)$  is in agreement with the proposed formulation (**Fig.8**). So the Zhang et al. model takes into account frequency and heating rate but not stress amplitude. De Jonghe et al. proposed a model in which the quantity of transformed phase per unit of time

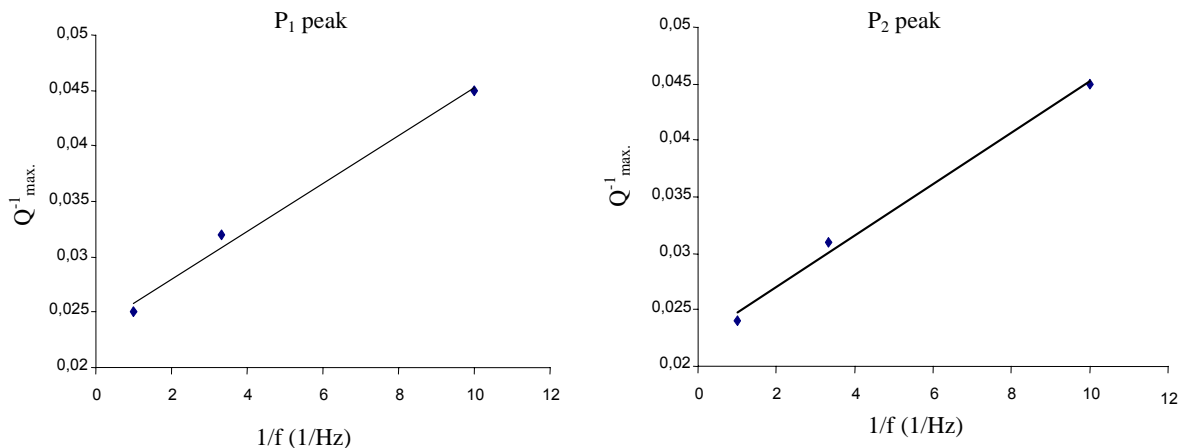
take into account both heating rate  $\dot{T}$  and applied stress amplitude  $\sigma$ , however the stress contribution is not available before a critical stress  $\sigma_c$ .

The quantity of transformed phase per unit of time ( $\dot{m} = f(\dot{T}, \sigma)$ ) is given by the relation :

$$\frac{dm}{dt} = \frac{\partial m}{\partial T} \frac{\partial T}{\partial t} + \frac{\partial m}{\partial \sigma} \frac{\partial \sigma}{\partial t}$$

The following relation is proposed to assess the internal friction:

$$Q^{-1} = \frac{A}{2\pi} \left[ \frac{\partial m}{\partial T} \cdot \frac{\partial T}{\partial t} \cdot \frac{1}{f} + \frac{4}{3} \cdot \sigma_0 \cdot \frac{\partial m}{\partial \sigma} \cdot \left\{ 1 - \left( \frac{\sigma_c}{\sigma_0} \right)^3 \right\} \right]$$



**Figure 6.**  $Q^{-1}_{max.}$  evolution versus  $(1/f)$  for  $P_1$  and  $P_2$  peaks for undoped PZT.

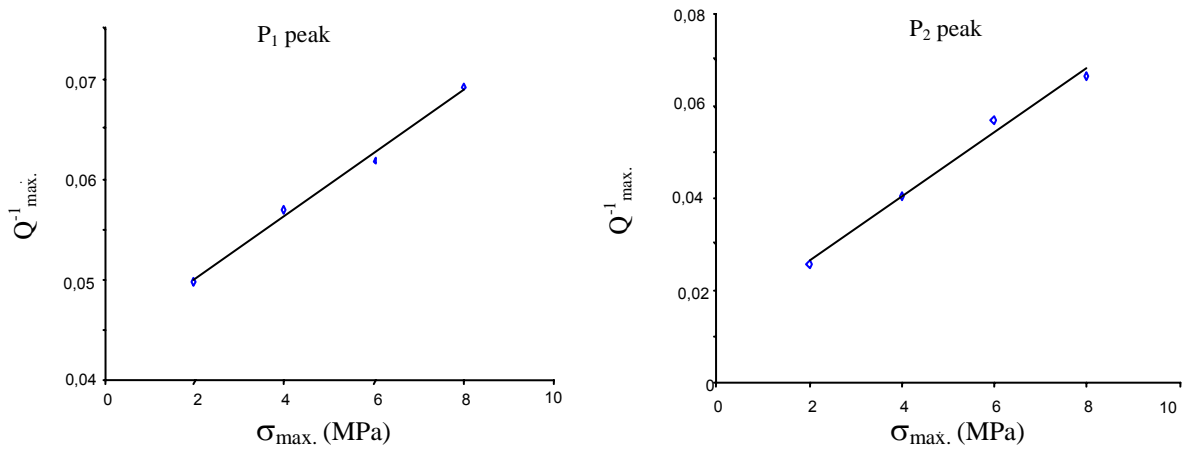


Figure 7.  $Q^{-1}_{max}$  evolution versus stress amplitude ( $\sigma_{max}$ ) for P<sub>1</sub> and P<sub>2</sub> peaks for undoped PZT.

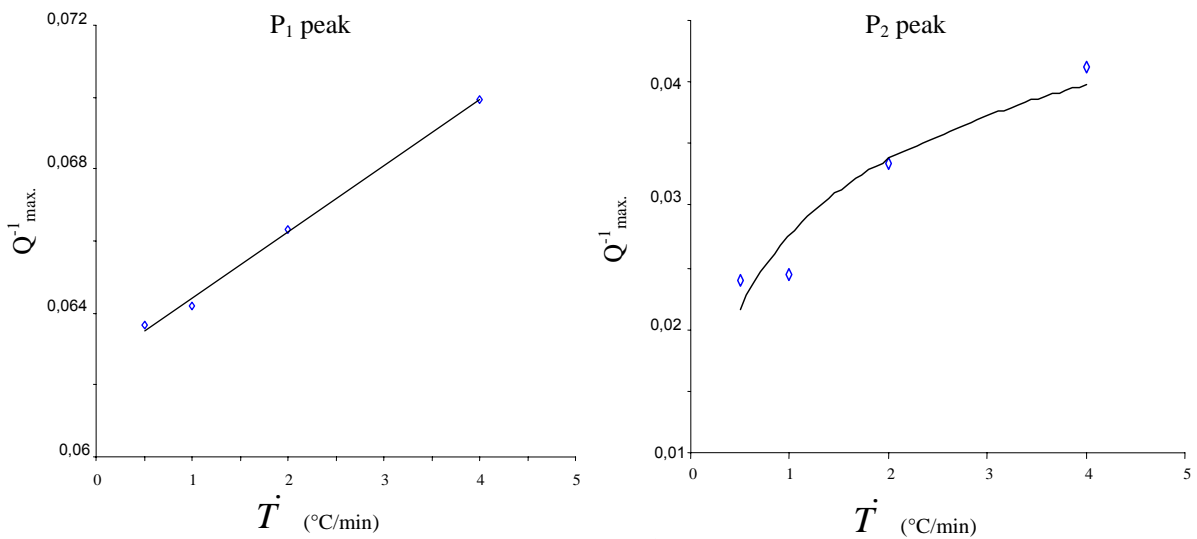


Figure 8.  $Q^{-1}_{max}$  evolution versus heating rate ( $\dot{T}$ ) for P<sub>1</sub> and P<sub>2</sub> peaks for undoped PZT.

Where:

**A** is a material constant,

$\frac{\partial m}{\partial T}$  Represents the relative transformed phase variation per unit of time,

$\frac{\partial T}{\partial t}$  is the heating rate,

$\omega$  is the frequency,

$\sigma_0$  is the applied stress amplitude,

$\frac{\partial m}{\partial \sigma}$  Represents the relative transformed phase variation per unit of stress; this term is rather related to the interfaces mobility.

Accordingly to the above models, the effect of potassium and niobium doping could be interpreted by the change of the nature of the transformed phase when doping. The change in the chemical composition of the starting transformed phase unit (or cell) by the introduction of aliovalent dopants could have as

a result the change of the kinetic and the strength of the phase transition process.

The presence of the P<sub>R</sub> shoulder is not clearly understand, we thought that it could be related to the anelastic phenomena represented at low frequencies by one or both R<sub>1</sub> and R<sub>2</sub> peaks. Further investigations are needed to better understand the P<sub>R</sub> shoulder.

## V. CONCLUSION

According to the P<sub>1</sub> and P<sub>2</sub> peaks temperatures and to the phase diagrams established for PZT solid solutions, one can notice the following considerations:

- The P<sub>1</sub> peak is attributed to the Curie transition –between cubic paraelectric phase and tetragonal ferroelectric phase– accompanied losses.

- The P<sub>2</sub> peak is attributed to the losses occurring during the phase transition between tetragonal and rhombohedral ferroelectric phases or to a more complex transition where

the monoclinic phase coexist with the tetragonal phase as shown by Noheda et al.<sup>4,5</sup> and Ragini et al.<sup>6</sup>.

- Both  $P_1$  and  $P_2$  peaks present a great similitude with a first order phase transition internal friction peak.

The introduction of potassium and niobium dopants changes the chemical composition of the starting transformed phase unit (or cell) and induces as a result the change of the nature of the phase transition process but the transition remains of first order.

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